

### Abstract

The desire for accurate navigation has been one of the great technology drivers since ancient times. Astronomy, timekeeping, magnetic sensors, the GPS system, MEMs, and spinning-mass gyroscopes are all familiar methods to measure position. The sensing of rotation by optical means was first demonstrated by Sagnac in 1913, and in 1925 Michelson and Gale measured the rotation of the Earth with a 2km loop interferometer. The Sagnac effect was relegated to being a physics curiosity, until the 1960s and the advent of the laser and optical fiber. One of the great achievements of navigation engineering was the harnessing of the Sagnac effect, to make practical and extremely sensitive yet rugged optical rotation sensors. The Sagnac effect is very small, and it is necessary to measure on the order of one part out of  $10^{30}$  to reach high-accuracy requirements. The design and manufacturing of practical optical gyroscopes is a tour-de-force of physics and engineering. Basic concepts such as symmetry, relativity, and reciprocity, and considerable interdisciplinary effort are needed in order to create a design such that every perturbation cancels out except rotation. Optical gyroscopes, and their research and production contracts, were an early driver for many ultra-high-performance optical technologies. Such commonplace items as low-scatter mirrors, ultrasonic machining of glass, lithium niobate integrated optics, polarization-maintaining fiber, superluminescent and narrow-linewidth lasers found their first major applications and customers in these sensors.

Presented to the IEEE SCV LEOS & IMS 5/27/2003. Preceding Image: Monolithic Ring Laser Gyro (MRLG). Copyright © 2000 Kearfoot Guidance and Navigation Corporation. Reproduced with permission.

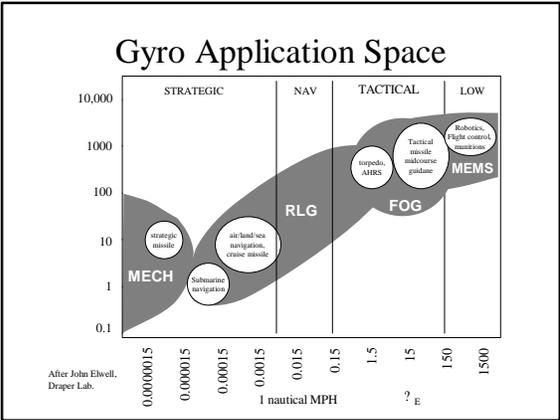
- ### Outline
- Gyroscope Basics and Applications
  - Gyroscope Specifications
  - Introduction to the Sagnac effect
  - The Ring Laser Gyroscope
  - Interferometric Fiber Optic Gyroscope
  - Resonant Fiber Optic Gyroscope
  - Waveguide Laser Gyroscope
  - Micro Optic Gyroscope

### Gyroscope Basics

Input | Axis (IA)

- Rate Gyro: Measures angular velocity  $\dot{\theta}$  about IA
- Rate-Integrating Gyro: Measures  $\int \dot{\theta} dt$
- Accelerometer
- Inertial Measurement Unit
  - Three or more Gyros
  - Three or more Accelerometers
  - Signal processing, navigation computer

- ### Types of Gyroscopes
- Spinning-Mass gyroscope
    - Exquisite single and dual-axis versions
    - Generally not a "strapdown" IMU
  - Vibratory gyroscope (Coriolis force)
    - Hemispherical, cylindrical, tuning-fork
    - MEMS gyroscope
  - Nuclear Magnetic Resonance
  - Optical Gyroscope



## Important Concepts

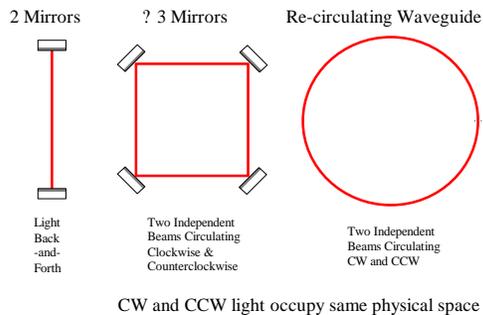
- Inertial Frame
  - Absolute reference system
- Reciprocity
  - Replace (t) with (-t) and (x,y,z) with (-x,-y,-z)
- Symmetry
  - Exploited whenever possible
- Special Theory of Relativity
  - Light in vacuum travels at  $3 \times 10^8$  meters/second
  - Light speed is independent of velocity of source

## Optical Interferometer

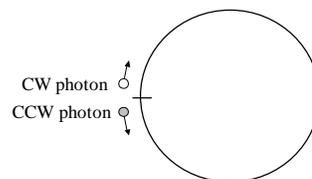


- Classic example of two precisely-aligned mirrors having ideally 100% reflection, separated by L
- Under certain conditions, constructive interference of multiple reflections permits light to pass through
- Transmission only for certain wavelengths ?  
 $\lambda/2 = L, \lambda = L, 3\lambda/2 = L, 2\lambda = L, \dots$
- Generally:  $m\lambda/2 = L$  where m is an integer, and propagation vector perpendicular to mirror coatings
- There will be m “Standing Waves” of size  $\lambda/2$

## Circulation in Interferometers



## Stationary Inertial Frame = Null

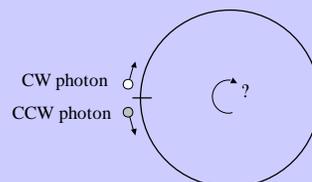


- Both photons experience exactly the same time-of-flight, resulting in destructive interference at the starting point
- $T_{cw} = T_{ccw} = 2R/c$  where R is the radius
- For optical fiber  $n \sim 1.5$  and  $T \sim 5$  microsecond/kilometer

## Rotating Inertial Frame

- Consider rotation rate to be ?
  - Units of radians/second,  $\omega > 0$  for clockwise
- Rigorous approach requires use of General Relativity, beyond the scope of this talk
- Use a simplified approach
  - Calculate  $\Delta L$  and  $\Delta T$
  - Refractive index = 1
  - Number of loops = 1

## Rotating Inertial Frame



- Both photons start at splice

### Rotating Inertial Frame

- Both photons start at splice
- Splice point rotated  $\theta$  radians, at tangential velocity  $R$
- $L_{cw} = 2R + R\theta$   $T_{cw} \triangleq cT_{cw}$
- $L_{ccw} = 2R - R\theta$   $T_{ccw} \triangleq cT_{ccw}$

$\theta = \frac{1}{c} \frac{4AR^2}{c^2} = \frac{4A}{c^2} R^2$

- Path Length:  $L = cT = 4A$
- Phase shift:  $\Delta\phi = (2\pi/\lambda)L = 8\pi A/\lambda$
- Phase shift is measured in rotating frame
  - $\theta$  can be deduced by measuring  $\Delta\phi$  via fringe shift, without knowledge of the absolute reference frame
- Example  $\lambda = 633\text{nm}$ ,  $A = 100\text{cm}^2$  ( $L \sim 35\text{cm}$ )
- Earth's rate  $\omega_e = 7.3 \cdot 10^{-5}$  radians/second
  - $L \sim 9.7 \cdot 10^{15}$  meters - a very small amount
  - $\theta \sim 9.6 \cdot 10^{-8}$  radians - just to measure Earth!
  - Need 1000x better than this for navigation.

## Ring Laser Gyroscope

### Ring Laser Gyroscope

- 3 or more mirrors in a stable alignment
- Sealed and filled with e.g. Helium and Neon
- Electrical discharge excites Helium and Neon ions, producing a population inversion of excited states
- These excited ions provide the gain medium
- With feedback, lasing commences when gain > loss

### Ring Laser Gyro Block

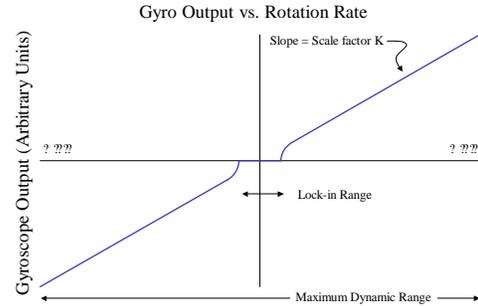
Image courtesy SVP

### Ring Laser Gyro Schematic

## Lasing in a Ring Cavity

- Two lasing beams of light
  - CW and CCW
  - Occupy the same physical space
- Use readout optics to interfere CW and CCW
- If stationary, beams have same wavelength  $\lambda$  ( $= c/f$ )
  - Cavity length is the same for both directions
  - Null output when CW and CCW interfere  $f_{cw} = f_{ccw}$
- For negligible rotation, beams also have same  $\lambda$ 
  - Lock-in effect, due to backscatter (coupled oscillator)
- For rotation above a lock-in rate  $\omega_L$   $f_{cw} \neq f_{ccw}$ 
  - Beat frequency is observed  $f_b = 4A\omega / \lambda L$

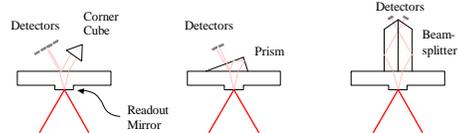
## Lock-In Effect in Optical Gyros



## Beat Frequencies

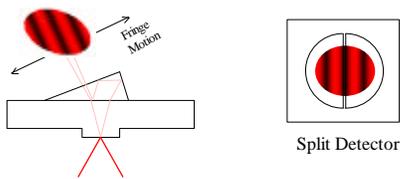
- Several approaches to avoid lock-in
  - Dither motor
  - Magnetic Mirror
- Beat frequency  $f_b = 4A\omega / \lambda L$
- In terms of phase shift
  - $\Delta\phi = 2\pi(f)t = 8\pi A\omega t / \lambda L$
- Example  $\lambda = 633\text{nm}$ ,  $A = 100\text{cm}^2$  ( $L \sim 35\text{cm}$ )
  - Optical frequency approximately  $f = c/\lambda \approx 4.74 \times 10^{14}$
- Earth's rate  $\omega_e = 7.3 \times 10^{-5}$  radians/second
  - $f_b \sim 13$  Hertz
  - $\Delta\phi \sim 83t$  radians

## RLG Readout Optics



- Unlike other mirrors, the readout mirror is designed to have  $< 100\%$  reflectivity, along with a slight transmission factor
  - This allows a small fraction of the circulating light to emit
- Attempt to overlay CW and CCW beams
  - Several approaches to achieve stable and robust implementation
- Often uses 2 or more silicon photodetectors
- Followed by low-noise and low-drift electronic preamplification
- Several signal processing approaches to extract  $\omega$  from  $\Delta\phi$

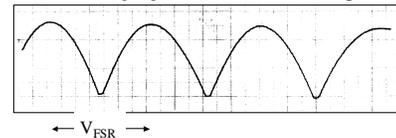
## Signal Processing



- Fringe counting (1 fringe corresponds to  $2\pi$ )
  - Since  $\Delta\phi = 2\pi(f)t$ , fringe is  $\Delta\phi / 2\pi = 4A\omega t / \lambda L$  ( $5.5 \times 10^5$  radians for 35cm)
- Fringe counting + sub-fringe interpolation
- Inverse tangent algorithm
- Numerous digital techniques

## Path Length Control

Laser output power vs. PZT drive voltage



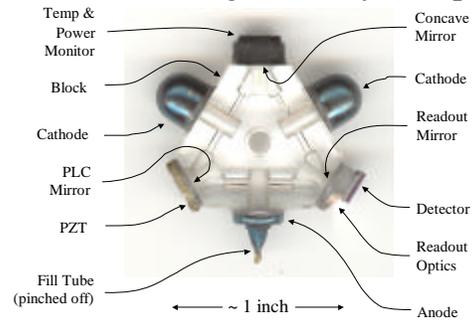
- Laser power fluctuates as a function of cavity length
- Free Spectral Range  $FSR = c/nL \sim 860\text{MHz}$  for 35cm
- One mirror pistons in and out several microns
- Piezoelectric transducer precisely controls mirror position
- Servo electronics stabilized cavity length

## Miniature Ring Laser Gyroscope

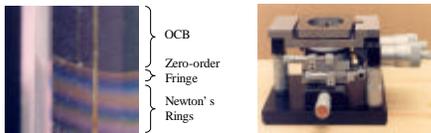


Image courtesy SVP

## Miniature Ring Laser Gyroscope



## Optical Contact Bonding



- Bonding mirrors to block without adhesive
- Demanding flatness, roughness specifications
- Ultra-clean assembly brings surfaces into contact
  - Newton's rings observed, zero-order fringe is grey
- If conditions are met, a slight pressure initiates bond
  - Van Der Waals force draws surfaces together if  $d$  is  $\ll 1$  micron
- Ageing produces strong, permanent, hermetic seal

## Honeywell GG1342 RLG



Image courtesy Honeywell

## Multiple Ring Laser Gyroscope

- Possible reduction from nine to six mirrors for 3-axis RLG
- Common block, gas reservoir, and cathode
- Complex machining, but overall parts savings
- Multiple scattering can cause interactions

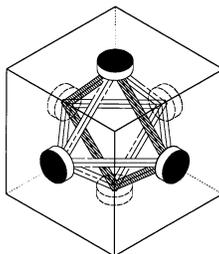
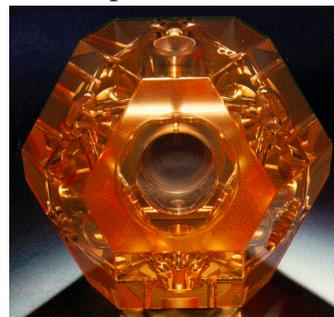


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## Multiple RLG Block



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## Multiple RLG in Action



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## Components

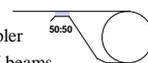
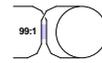
- RLG block
  - Low-expansion material: ULE, Zerodur, or Cervit
  - Filled with proprietary cocktail of He<sub>2</sub> and Ne<sub>2</sub> isotopes
- Mirrors
  - Low scatter is important
  - May have path-length control
- Readout Optics
- Photodetectors
- Dither motor
- Anode/Cathode/Fill tube/Getters

## Fiber Optic Gyroscope

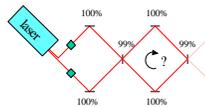
RFOG  
IFOG

## Fiber Optic Gyroscope

- Resonant Fiber Optic Gyroscope (RFOG)
  - Replace cavity with optical fiber
  - Use high-splitting ratio fiber coupler
  - At resonance, light can circulate
  - Uses narrow-linewidth (coherent) optical sources
- Interferometric Fiber Optic Gyroscope (IFOG)
  - Longer coil of optical fiber
  - Use 50/50 splitting ratio fiber coupler
  - Topology produces CW and CCW beams
  - Uses broad-linewidth (incoherent) optical source



## Passive Optical Gyro



- Resonant Fiber Optic Gyroscope (RFOG)
  - Replace cavity with optical fiber
  - Use high-splitting ratio fiber coupler
  - At resonance, light can circulate
  - Uses narrow-linewidth (coherent) optical sources

## FOG Building Blocks

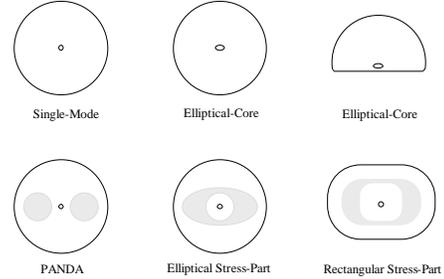


- Polarization-Maintaining Fiber Coupler
- Fiber polarizer
- PZT Phase modulator
- Fiber depolarizer
- Pigtailed optical isolator
- Planar lightwave circuit
- Optical detectors
- PM optical fiber coil

## Polarization-Maintaining Fiber

- “Single-mode” fiber actually propagates 2 modes
  - Two orthogonally polarized modes, e.g. x- and y-mode
  - Ideally travel at the same propagation velocity
  - Small perturbations can cause coupling between x- and y-modes
  - Small perturbations can rotate the local fiber x- and y-axis randomly
- PM fiber has anisotropy to break modal degeneracy
  - One mode has a higher velocity than the other
  - Well-defined principal axes of PM optical fiber
  - X- and y-modes can have many dB of isolation
  - Small, random, perturbations have negligible influence on coupling
- Techniques
  - Elliptical-core optical fiber (3M, D-shaped fiber)
  - Stress-rod fiber (PANDA, Bow-Tie, elliptical cladding)
  - Material (side-pit fiber, photonic bandgap fiber)
  - Need special components, and splicing equipment with axial alignment

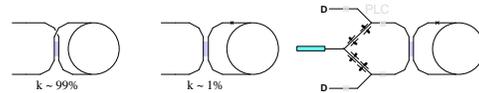
## Anisotropy – Breaking Symmetry



## Phase and Frequency Shifter

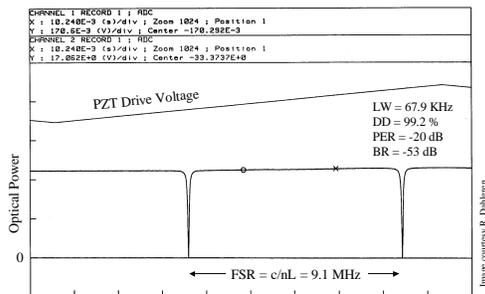
- Fiber-wrapped PZT stretcher
  - Piezoelectric cylinder
- Electro-Optic phase modulator
  - Lithium Niobate PLC
- Acousto-Optic frequency shifter
  - Uses Doppler effect. Difficult to pigtail
- Serrodyne modulator (quasi-frequency shifter)
  - Lithium Niobate PLC phase modulator
  - Driven with sawtooth wave at constant 2 $\pi$ -amplitude
  - Slope of sawtooth = frequency shift
  - High-speed analog electronics needed

## RFOG Architectures

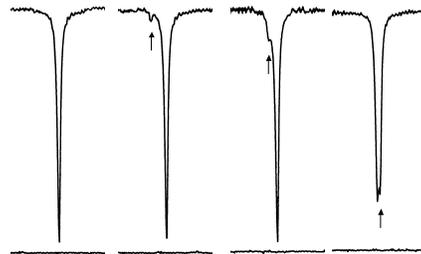


- Resonant Fiber Optic Gyroscope (RFOG)
  - Spliced assembly of low-loss PM fiber coil and PM coupler
  - High-splitting ratio fiber coupler, optimized  $k = 1$ -Loss
  - Alternately, low-splitting ratio coupler, set  $k = \text{Loss}$
  - Can also add 2<sup>nd</sup> coupler and operate in transmission mode
- Planar lightwave circuit (PLC)
  - Need electro-optic effect -  $\text{Ti:LiNbO}_3$  for phase/frequency modulator
  - Discrete or distributed polarizer
  - Splitter with low asymmetry, good polarization performance
  - Pigtailed to PM fiber, packaged to meet aerospace requirements
- Tunable narrow-linewidth source, significant signal processing

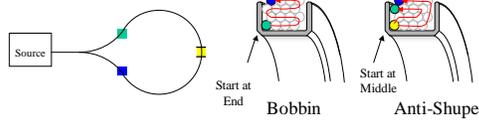
## Transmission of RFOG Cavity



## Polarization in RFOG Cavity



## Coil Winding Style



- For coherent source – only narrow range of coil will suffer parasitic effects due to backscattering
- Exploit symmetry
  - Wind coil from center, alternating layers such that equidistant fibers are physically adjacent
  - Provides immunity to thermal and vibration perturbations that are slow with respect to transit time
  - Called quadropole or anti-Shupe winding pattern

## Coil Winding Operation

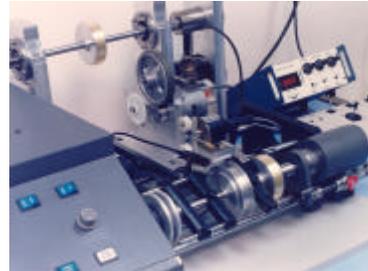


Image courtesy R. Dalglem

## 400m Anti-Shupe Coil (unpotted)

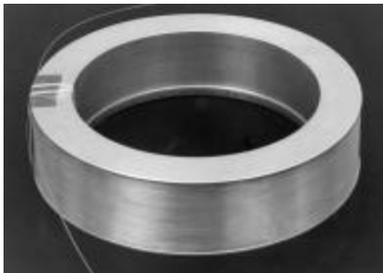


Image courtesy R. Dalglem

## Resonant Fiber Gyroscope



Image courtesy Draper Lab

## IFOG Architectures



- Minimum-configuration IFOG
  - Uses polarizer (P) and 2<sup>nd</sup> splitter for detector (D)
  - Sinusoidal phase modulation with PZT fiber stretcher
  - Unbiased operation. At zero rotation  $\gamma = 0$
  - Open-Loop IFOG operation possible
- 3:3 splitter IFOG (not shown)
- PLC Implementation
  - Needs Ti:LiNbO<sub>3</sub> PLC for frequency shifter
  - Phase modulator and one splitter also incorporated
  - Nonreciprocal  $\pi/2$  phase shift introduced.
  - At zero rotation, biased at maximum sensitivity point  $\gamma = \pi/2$

## Optical Source for IFOG

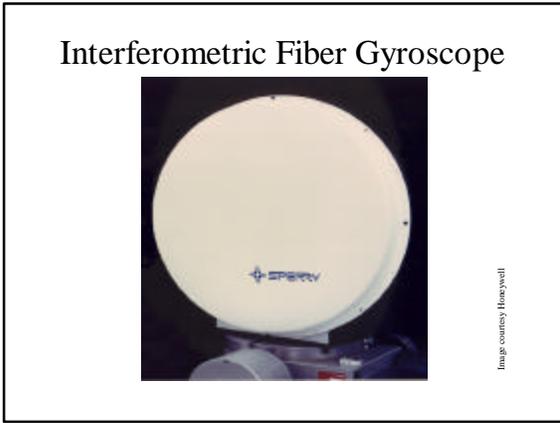
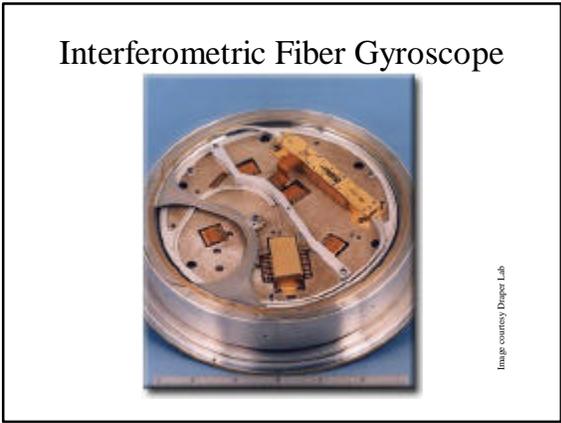
- Low-coherence source reduces parasitic interference from scattering points and distributed (Rayleigh) scattering
  - Sub-threshold LD
  - Edge-emitting LED
  - Superluminescent Diode
  - Amplified Spontaneous Emission
  - Amplified broadband source
- Can share high-power source between several gyroscopes
- Need to control optical power accurately
- Need to match CW and CCW power to avoid Kerr effect
- Need to control optical center  $\gamma$  accurately

### Open Loop Signal Processing

- Open loop
  - Unbiased operation  $\theta = 0$
  - Minimum sensitivity point for small  $|\theta|$
  - Sinusoidal oscillator at frequency  $f_0$  optimized for transit time
  - Optical phase modulation at optimum amplitude
  - Use lock-in amplifier (LIA) to measure RMS voltage at  $f_0$
  - Use lock-in amplifier (LIA) to measure RMS voltage at  $2f_0$
  - Ratio of two RMS voltages yields magnitude and sign of  $\theta$
  - Limited dynamic range

### Closed Loop Signal Processing

- Closed loop IFOG
  - Needs Ti:LiNbO<sub>3</sub> PLC for frequency shifter
  - Phase modulator and one splitter also incorporated
  - Nonreciprocal  $\pi/2$  phase shift introduced. At zero rotation  $\theta = -\pi/2$
  - Servo-electronics locks operating point to  $-\pi/2$  maximum sensitivity point
  - Servo-electronics differentially drives frequency shifters to keep on null
  - Servo-electronics yields magnitude and sign of  $\theta$
  - Wide dynamic range



### Integrated Optic

WLG  
 MOG  
 IORS

- ### Waveguide Laser Gyroscope
- Integrated optic implementation of RLG
    - Rare-earth doped waveguide ring cavity
    - Pumped at pumping wavelength
    - Mode competition between the two counter-propagating beams prohibit functioning
  - Brillouin Effect gyroscope
    - Demonstrated at MIT
  - Squeezed-light gyroscope
    - Demonstrated at MIT

## Micro-Optic Gyroscope

- Northrop Corp in the 1980s
- Integrated optic implementation of RFOG
  - PLCs have higher attenuation than fiber
  - PLCs had limited length of waveguide
  - Surface acoustic wave (SAW) optical frequency shifters
  - 1-100 degrees/hour performance

## Wafer with MOG Chips

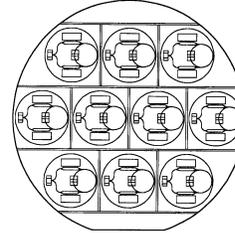


Image courtesy Springer-Verlag © 1993

## Integrated Optic Rate Sensor

- Rice Systems in the 2000s
- Integrated optic implementation of IFOG
  - Improved PLC technology
  - PLCs had limited length of waveguide
  - Open-loop architectur



Image courtesy Rice Systems